

In memoriam
CHRISTIAN PELECUDI, Vicepresident of IFToMM

PASSIVE MODULAR GROUPS WITH EIGHT ELEMENTS FROM INVERSE STRUCTURAL MODELING OF PLANAR LINKAGES

ADRIANA COMĂNESCU¹, DORU BOBLEA², ANTONIA ONACA³

Abstract. Bi-mobile mechanisms commonly used in robotics are obtained as structural solutions from plane linkages with five degrees of freedom, in which the basis and effector are nominated and two active kinematic pairs of the system are positioned. The basis and the effector are determined by inverse structural modeling, the inverse model consisting exclusively of passive modular groups. It is obtained by connecting the effector with plane motion dependent on two independent parameters through a virtual kinematic pair at the basis canceling the degree of mobility. The placement of active pairs is achieved by direct structural modeling, the direct model consisting of active and, eventually, passive modular groups. A mechanism performing with precision and accuracy of motion must have the inverse model and the direct model consisting of a minimum number of modular groups, as appropriate passive or active ones. The optimal inverse model is always a Baranov truss, from which the elimination of the basis results a single passive modular group. Bi-mobile mechanisms with three independent contours are obtained from the 40 kinematic chains with five degrees of freedom and three independent contours mentioned in the literature [Appendix 1]. They have a number of 8 mobile elements and 11 lower kinematic pairs, and the optimal inverse models, characterized by 9 elements and 12 kinematic pairs being Baranov trusses. The number of passive modular groups with 8 elements obtained from a Baranov truss with nine elements is $C_9^8 = C_9^1 = 9$, from which indistinct solutions due to symmetrical elements are eliminated. Thus, there are 188 structures, of which 95 ones are found in the solutions of the inverse models mentioned and are specially marked.

Key words: bi-mobile linkage, bi-mobile robot mechanism, optimal solution, baranov truss, passive modular group, inverse modelling, direct modelling.

¹ “Politehnica” University of Bucharest, Romania

² Atlantic Technological University, Galway, Ireland

³ “Carol Davila” University of Medicine and Pharmacy Bucharest, Romania

1. INTRODUCTION

The structural synthesis of bi-mobile plane mechanisms based on kinematic chains with five degrees of freedom required the selection of base and effector elements in the chain, achieved by inverse modeling [6, 7, 11]. The virtual connection to the base of the effector with plane motion dependent on two independent parameters [8, 11] leads to the cancellation of the mobility of the structure. The solutions are recorded in a base – effector square and symmetric matrix (nxn) with Boolean values in which n signifies the number of elements of the chain [8].

In previous papers, inverse models have been analyzed. Due to the degree of null mobility, there are constituted by passive modular groups (Assur). In the case of linkages with 9 elements and three independent contours, the inverse model can have one of the following passive structures: 2+2+2+2, 2+2+4, 2+4+2, 4+2+2, 2+6, 6+2, 8 [7,8]. The optimal inverse models are equivalent to Baranov trusses with 9 links, which have a single passive modular group with 8 elements. Such modular groups are found in literature exclusively in the case of structural models dedicated to the selection of the base and effector of bi-mobile mechanisms [1–4, 12–23].

The number of passive modular groups with 8 elements obtained from a Baranov truss with nine elements is $C_9^8 = C_9^1 = 9$, from which non-distinct solutions due to symmetric elements are retained. This paper includes aspects related to these passive modular groups of structural modular inverse models.

In the classical mechanism theory literature the first passive modular groups were used in the structural analysis and synthesis of plane mechanisms, especially mono-mobiles using their fundamental (Assur) principle of formation. These were correlated with the Baranov trusses with three links (BT 1), five (BT 2, BT3) and seven ones (BT 4, BT 5) from which they are deduced.

In recent years, Baranov trusses have come to the attention of researchers [4]. The structural synthesis of bi-mobile plane mechanisms based on kinematic chains with five degrees of freedom required the selection of base and effector elements in the chain, achieved by inverse modeling [8–11].

The advantage of such a structure lies in the high precision with which the trajectory of the effector end is achieved.

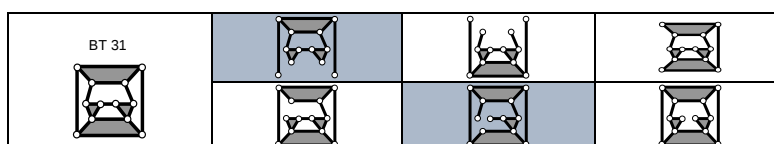
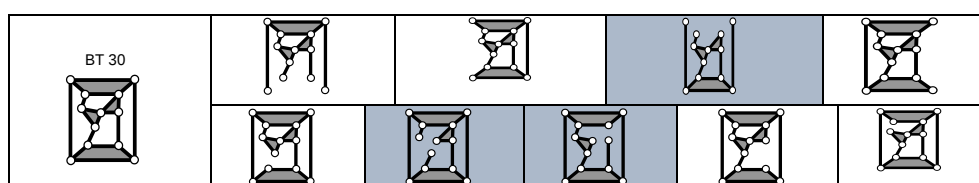
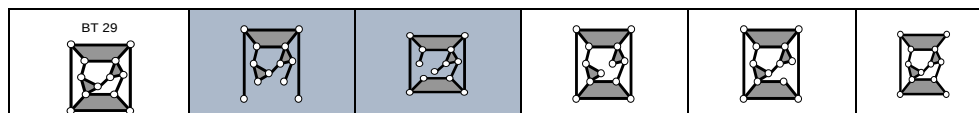
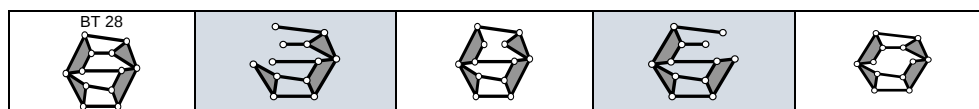
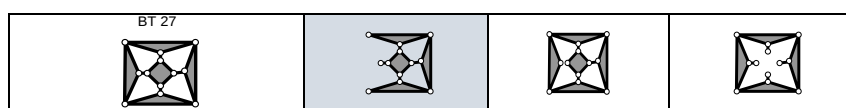
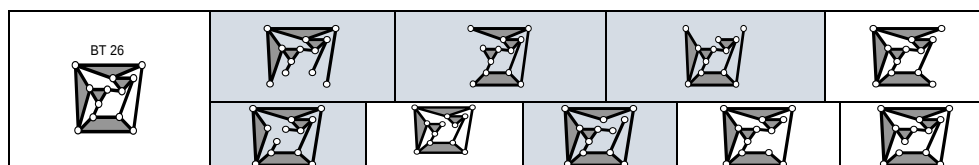
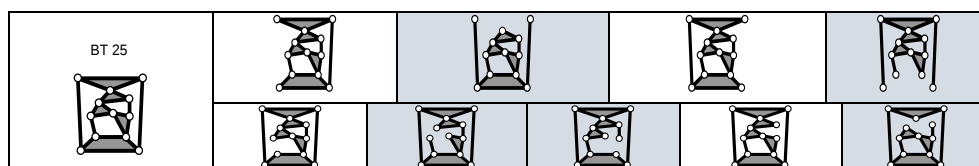
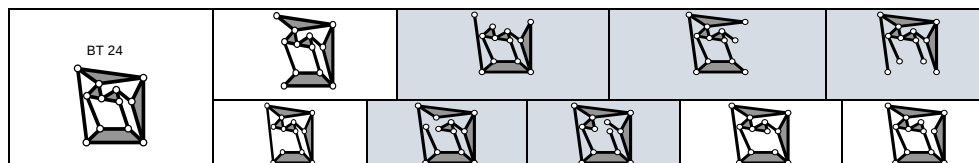
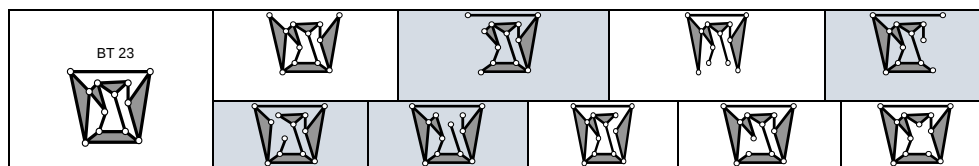
2. STRUCTURAL SOLUTIONS FOR PASSIVE GROUPS WITH EIGHT ELEMENTS

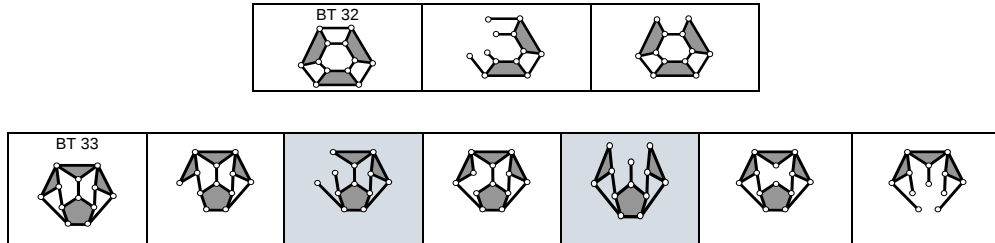
Passive modular groups with eight elements are obtained as structural solutions from Baranov trusses with 9 elements named BT6 – BT33. These are shown in Table 1, which synthesizes the distinct ones for each of them, marked those found in the inverse models of bi-mobile mechanisms and three independent contours.

Table 1

Passive modular groups with eight elements

The image displays a series of 20 visual puzzles arranged in a 4x5 grid. Each puzzle is a 2x2 grid of shapes. The first shape in each puzzle is labeled BT 6 through BT 14. The shapes are 3D wireframe models of polyhedra, some with internal structures. The background of the 2x2 grid is divided into four quadrants, some of which are shaded light blue. The goal is to determine the missing shape in the bottom-right quadrant of each 2x2 grid.





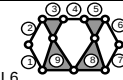
Consequently, from the Baranov BT6 – BT33 trusses with 8 elements emerge 188 passive modular groups with 9 elements, 95 of which are found in the optimal inverse models of bi-mobile mechanisms and three independent contours exposed below.

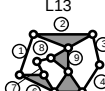
3. PASSIVE GROUPS WITH EIGHT LINKS APPLIED TO OPTIMAL INVERSE MODELS OF BI-MOBILE AND THREE LOOPED MECHANISMS

Following the solutions of the passive groups highlighted in Table 1, the optimal base-effector solutions $A(i,j)$ for bi-mobile mechanisms and three independent contours (Table 2) obtained by inverse modelling of the L_j related kinematic chains [appendix 1].

Table 2

Passive modular groups with eight elements in optimal structural solutions for basis-effector

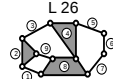
	Baranov truss	Passive structural groups with 8 elements					
		Kinematic linkage L_j					
		Optimal basis i – effector j solutions $A(i,j)$					
1.	BT 6						
		 L3	 L6		 L3		
		A(3,7)	A(2,6)		A(7,3)		
2.	BT 7						
		 L13	 L15	 L15	 L27	 L35	 L35

		A(4,8)	A(4,8)	A(8,4)	A(1,7)	A(8,2)	A(2,8)
3.	BT 8						
							
		A(3,7)	A(5,2)	A(1,5)	A(2,6)	A(7,3)	A(2,5)
4.	BT 9						
							
		4A(1,6)	A(6,1)	A(1,7)	A(3,9)	A(1,4)	A(9,3)
5.	BT 10						
							
		A(1,6)	A(2,6)	A(6,1)	A(6,2)	A(1,5)	
							
							
		A(5,1)	A(6,3)	A(5,2)	A(3,6)	A(2,5)	
6.	BT 11						
							
		A(3,7)					
7.	BT 12						
							

		A(3,8)	A(4,9)	A(9,4)	A(7,2)	A(6,7)	A(7,6)	A(2,7)
8.	BT 13							
		L20 	L25 	L20 	L25 	L 32 	L 32 	
		A(2,5)	A(1,4)	A(5,2)	A(4,1)	A(4,1)	A(1,4)	
9.	BT 14							
		L3 	L5 	L3 	L19 	L5 	L14 	
		A(3,6)	A(8,3)	A(6,3)	A(1,7)	A(3,8)	A(4,1)	
		L11 	L30 	L11 	L14 	L19 	L 30 	
		A(1,6)	A(4,1)	A(6,1)	A(1,4)	A(7,1)	A(1,4)	
10	BT 15							
		A(1,9)	A(9,1)					
	BT 16							
		L17 	L19 	L17 	L 37 	L28 		
		A(2,6)	A(1,8)	A(6,2)	A(1,5)	A(5,2)		
		L19 	L28 	L 37 				

		A(8,1)	A(2,5)	A(5,1)
12	BT 17			
		A(1,5)	A(4,1)	A(9,5)
13	BT 18	A(1,4)	A(6,2)	A(5,9)
		A(1,7)	A(4,8)	A(2,5)
14	BT 19			
		A(7,1)	A(8,4)	A(5,2)
15	BT 20			
		A(1,6)	A(3,6)	A(6,1)
15	BT 20	A(2,6)	A(2,6)	A(6,2)
		A(6,2)	A(3,6)	A(7,2)

16 .	BT21						
		A(1,6)		A(2,5)		A(6,1)	
17 .	BT22						
		A(1,6)		A(4,7)		A(6,1)	
18 .	BT23						
		A(2,7)		A(6,1)		A(7,2)	
		A(2,5)		A(6,2)		A(2,6)	
19 .	BT 24						
		A(2,6)		A(6,2)		A(1,4)	
20 .	BT 25						
		A(1,6)		A(9,3)		A(6,1)	
21 .	BT 26						
		L21		L23		L27	

									
22 .	BT 27								
		L12							
		A(1,5)							
23	BT 28								
									
		L40							
24	BT 29								
									
		L26							
25	BT 30								
									
		L22		L23		L22		L23	
		A(1,5)		A(1,5)		A(1,5)		A(5,1)	
26	BT31								
									
		L34							
27 .	BT 33								
									
		L39							
		A(2,6)				A(6,2)			

Two manipulators (Fig. 1 and Fig. 2), obtained from solutions mentioned in Table 2 are designed.

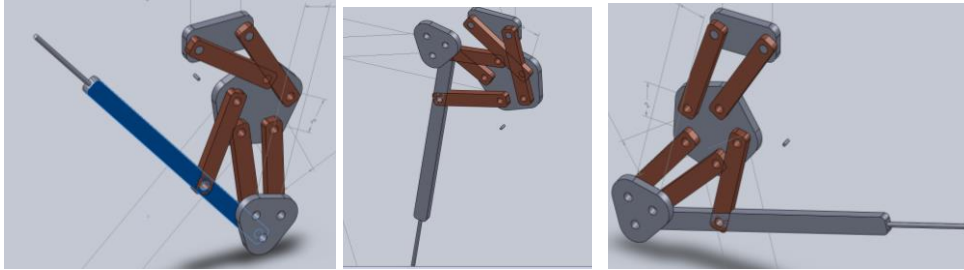


Fig. 1 – Manipulator based on linkage L39 with basis 2 and effector 6.

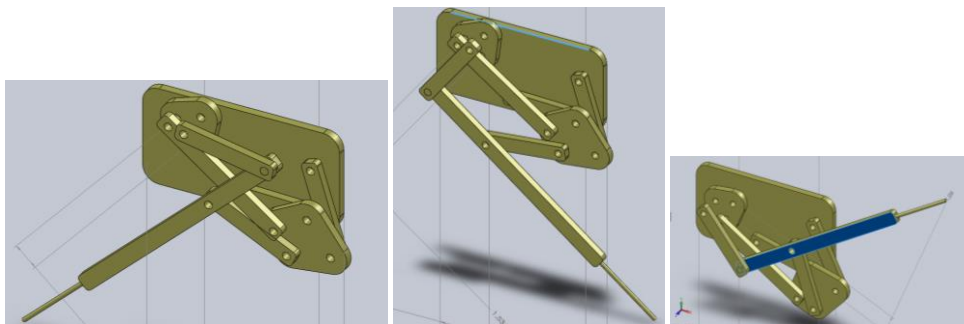


Fig. 2 – Manipulator based on linkage L34 with basis 1 and effector 5.

4. CONCLUSIONS

The paper highlights two aspects in close connection with the theory of mechanisms and robots.

Thus, the 13 passive modular groups called classic Assur groups obtained from Baranov BT1 – BT6 trusses are completed with the assembly of those with 8 elements detached from Baranov trusses B6 – B33 (Table 1). They were not interested in the synthesis of mechanisms and found their importance in inverse modeling of bi-mobile linkages and three independent contours, by which they nominate the base and effector for robot mechanisms with two degrees of mobility [5–8].

Also, the optimal base-effector solutions for bi-mobile robot mechanisms are highlighted, which are based on inverse modeling on passive modular groups with 8 elements (Table 2). They are an inexhaustible source of technical solutions for researchers and designers in the field. Two variants of robot mechanisms that fit these requirements are presented.

Received on March 12, 2024

REFERENCES

1. ARTOBOLSKII, I. I., *Theorie des mecanismes et des machines*, Editions Mir, Moskova, 1977.
2. ASSUR, L.V., *Investigation of Plane Hinged Mechanisms with Lower Pairs from the Point of View of their Structure and Classification: Part I, II*, Bull. Petrograd Polytech. Inst., **20** (1913), pp. 329–386; Bull. Petrograd Polytech. Inst., **21** (1914), pp. 187–283; **21–23**, 1914–1916.
3. BARANOV, G. G., *Classification, Structure, Kinematics and Kinetostatics of Mechanisms with First Kind Pairs*, Proc. Seminar on TMM, **2**, 46, pp. 15–39, 1952.
4. CHU, J., CAO, W., YANG, T., *Type Synthesis of Baranov Truss with Multiple Joints and Multiple-Joint Links*, Proc. ASME Design Engineering Technical Conference, September 13–16, 1998, Atlanta, Georgia.
5. COMĂNESCU, Adr., BOBLEA, D., DUGĂEȘESCU, I., SOARE, G., *Fixed Sequence Agricultural Robot Functional Characteristics*, Proc. of SYROM 2022 & ROBOTICS 2022, Springer Nature Switzerland AG, 2022, pp. 57–66.
6. COMĂNESCU, Adr., DUGĂEȘESCU, I., BOBLEA, D., GHEORGHITA, A., *Bi-mobile Mechanisms Modelling for Variable Sequence Robots*, Proc. of SYROM 2022 & ROBOTICS 2022, Springer Nature Switzerland AG, 2022, pp. 67–76.
7. COMĂNESCU, Adr., COMĂNESCU, D. & col., *Mechanisms – Analysis and Synthesis – Modelling, Simulation and Optimization of Mechanical Systems*, “Politehnica” Press, Bucharest, 2021.
8. COMĂNESCU, Adr., COMĂNESCU, D. & col., *Modelling and Optimization of Mechanisms and Mechanical Systems in Robotics*, “Politehnica” Press, Bucharest, 2023.
9. COMĂNESCU, Adr., BĂNICĂ, E., COMĂNESCU, D., *Human inferior member model for a medical functional recovering system*, 8th World Congress of Biomechanics, 8–12 July 2018, Dublin, Ireland.
10. COMĂNESCU, Adr., DUGĂEȘESCU, I., BOBLEA, D., UNGUREANU, L., *Multifunctional Medical Recovery and Monitoring System for the Human Lower Limbs*, Sensors Journal, **19**, 22, Article Number: 5042, DOI: 10.3390/s19225042, 2019.
11. COMĂNESCU, Adr., ZALESCHI, C., *Bi-mobile mechanisms designed by means of their inverse models*, 2016 International Conference on Applied Mechanics Electronics and Mechatronics Engineering (AMEME 2016) May 28–29, Beijing, China, 2016, pp. 279–285.
12. CROSSLEY, F.R.E., *The Permutations of Kinematic Chains of Eight Members or Less From the Graph-Theoretic Viewpoint*, Developments in Theoretical and Applied Mechanics, **2**, pp. 467–486, 1967.
13. HAIN, K., *Getriebesystematik*, Beitrag nr.BW 881 des VDI-Bildungswerks, Düsseldorf, 1965.
14. HAHN, E., SHAI, O., *A Single Universal Construction Rule for the Structural Synthesis of Mechanisms*, Proc. of ASME Design Engineering Technical Conferences, August 21–24, 2016, Charlotte, NC.
15. HAHN, E., SHAI, O., *Construction of Baranov Trusses Using a Single Universal Construction Rule*, Proc. of ASME Design Engineering Technical Conferences, August 21–24, 2016, Charlotte, NC.
16. HESSELBACH, J., THOBEN, R., PITTSCHELLIS, R., *Parallelroboter für hohe Genauigkeiten*, wt-Produktion und Management, 86, 1996.
17. KERLE, H., PITTSCHELLIS, R., *Einführung in die Getriebelehre*, B.G.Teubner, Stuttgart, 1998.
18. MANOLESCU, N.I., *A Method Based on Baranov Trusses, and Using Graph Theory to Find the Set of Planar Jointed Kinematic Chains and Mechanisms*, Mech. Mach. Theory, **8**, 1, pp. 3–22, 1973.
19. MANOLESCU, N.I., *A Unified Method for the Formation of all Planar Jointed Kinematic Chains and Baranov Trusses*, Environment and Planning B, **6**, 4, pp. 447–454, 1979.
20. PELECUDI, Chr., *Bazele analizei mecanismelor*, Edit. Academiei RPR, Bucharest, 1967.
21. ROJAS, N., THOMAS, F., *On closed-form solutions to the position analysis of Baranov trusses*, Mechanism and Machine Theory, **50**, pp. 179–196, 2012.
22. SONAWALE, K.H., MCCARTHY, J.M., *Synthesis of eight-bar linkages by constraining a 6R loop*, Mechanism and Machine Theory, **105**, 2016.
23. VOLMER, J., *Getriebetechnik-Grundlagen*, 2.Aufl., Berlin, München, Verlag Technik, 1995.

APPENDIX

Bi-mobile and three looped linkages

